

## **Thermal Segmentation of Mid-Ocean Ridge Transform Faults**

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### **Introduction**

The equation for  $A_U$ , the seismogenic area for an unsegmented mid-ocean ridge transform fault (Eq. 7 in the paper):

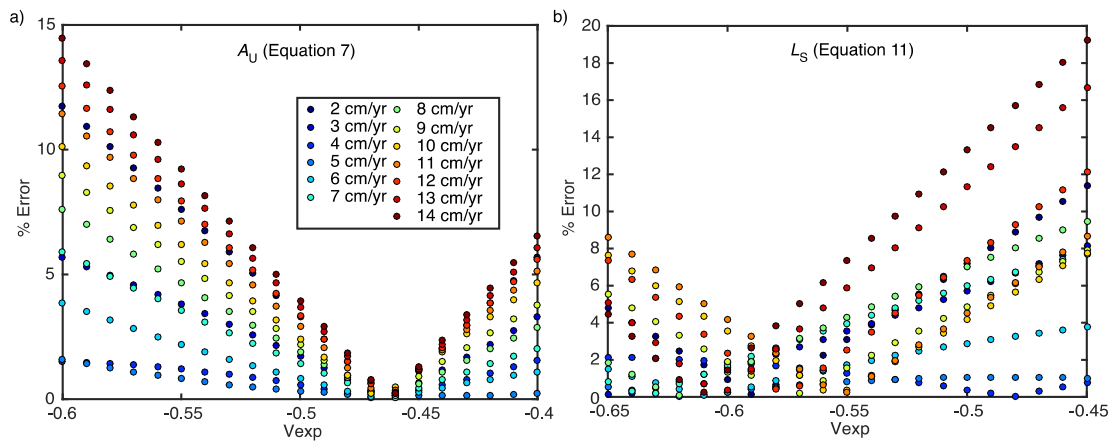
$$A_U = C_{600} L_T^{1.5} V^{-0.5}$$

and the equation for  $L_S$ , the critical step-over length (Eq. 11 in the paper):

$$\widetilde{L}_S = C_0 \frac{L_1^{1.5} + L_2^{1.5} - 0.1|L_1 - L_2|^{1.5}}{L_1 + L_2} V^{-0.6}$$

have the same exponent on the length terms ( $L_T$ ,  $L_1$  and  $L_2$ ), but different exponents on the slip rate ( $V$ ). In order to show the significance of the exponent on the slip rate ( $V_{exp}$ ) for  $A_U$  and  $\widetilde{L}_S$ , we plot a range of exponent values versus the computed percent error between  $A_U$  and  $\widetilde{L}_S$  derived from the model, and  $A_U$  and  $\widetilde{L}_S$  predicted from the scaling

relation with the given exponent value for the full range of slip rates (2 cm/yr to 14 cm/yr) for a segmented fault system composed of two 50-km long faults (Fig. S1). In figure S1, panel (a) shows the  $V_{exp}$  versus percent error plot for  $A_U$  and panel (b) shows the same plot for  $\widetilde{L}_S$ . In the case of the scaling relation for  $A_U$ , the percent error is minimized at a  $V_{exp}$  value of -0.46 for all slip rates. In the case of the scaling relation for  $\widetilde{L}_S$ , the percent error is minimized at different  $V_{exp}$  values depending on the slip rate. The spread in the percent error values, however, is minimized for a value of -0.59. The  $V_{exp}$  exponent values are then rounded to two significant digits (-0.5 and -0.6, respectively) for use in the  $A_U$  and  $\widetilde{L}_S$  equations. The use of a  $V_{exp}$  value of -0.5 in the equation for  $A_U$  matches the theoretical value derived from the halfspace cooling model [Boettcher & Jordan, 2004]. Rounding this term results in a negligible increase the percent error for both  $A_U$  and  $\widetilde{L}_S$ .



**Figure S1.** Percent error versus the exponent on the slip rate term ( $V$ ) in the equations for  $A_U$  (a) and  $\widetilde{L}_S$  (b) for a segmented fault composed of two 50-km long fault segments. Data points are colored by slip rate.

For each value of the slip rate exponent tested in the scaling relations in figure S1, a new constant is computed,  $C_{600}$  for  $A_U$  and  $C_0$  for  $\widetilde{L}_S$ . In the equation for  $A_U$ , a  $V_{exp}$  value of -0.5 corresponds to a  $C_{600}$  value of  $6.87e-4$  (m/s) $^{(1/2)}$ . For  $\widetilde{L}_S$  with a  $V_{exp}$  value of -0.6,  $C_0 = 1.35e-4$  m $^{1.1} s^{-0.6}$ . We round these numbers to two significant digits as well ( $6.9e-4$  and  $1.4e-4$ , respectively) to simply the equations and preserve consistency in the significant digits.