Flow separation effects on shoreline sediment transport

Julia Hopkins, MIT-WHOI Joint Program in Civil and Environmental Engineering, Cambridge, MA

Steve Elgar and Britt Raubenheimer, Woods Hole Oceanographic Institution, Woods Hole, MA

Corresponding author: J. Hopkins, MIT/WHOI Joint Program, 15 Vassar Street Rm 48-208, Cambridge, MA, 02139 (hychenj@mit.edu)

Abstract

Field-tested numerical model simulations are used to estimate the effects of an inlet, ebb shoal, wave height, wave direction, and shoreline geometry on the variability of bathymetric change on a curved coast with a migrating inlet and strong nearshore currents. The model uses bathymetry measured along the southern shoreline of Martha's Vineyard, MA, and was validated with waves and currents observed from the shoreline to ~10-m water depth. Between 2007 and 2014, the inlet was open and the shoreline along the southeast corner of the island eroded ~200 m and became sharper. Between 2014 and 2015, the corner accreted and became smoother as the inlet closed. Numerical simulations indicate that variability of sediment transport near the corner shoreline depends more strongly on its radius of curvature (a proxy for the separation of tidal flows from the coast) than on the presence of the inlet, the ebb shoal, or wave height and direction. As the radius of curvature decreases (as the corner sharpens), tidal asymmetry of nearshore currents is enhanced, leading to more sediment transport near the shoreline over several tidal cycles. The results suggest that feedbacks between shoreline geometry and inner-shelf flows can be important to coastal erosion and accretion in the vicinity of an inlet.

1. Introduction

Sediment transport on shorelines is affected by wave-orbital velocities, breaking-wave-driven currents, tidal currents, and inlet flows. In particular, inlet flows can interrupt alongshore sediment transport, resulting in sediment deposition inside the bay (flood tide delta), in the ocean near the inlet mouth (ebb-tide delta or shoal) or farther offshore [1–4, references therein and many others]. Erosion downstream of the inlet is possible owing to inlet-induced reduction in alongshore sediment supply. The inlet influence can extend for more than 10 km along the coast [5], although it often extends less than 4 km [4–7]. The inlet region of influence depends on many factors, including the geometry of the ebb shoal and main inlet channel [8], the offshore bathymetry [9,10], wave climate [11,12], tidal prism [4,13], and the presence of headlands [14,15].

Traditional knowledge associates increased sediment transport around the shoreline at Wasque Point on the southeast corner of Martha's Vineyard, MA, USA (Figure 1) with the opening of the nearby Katama Inlet [16]. Katama Inlet breached in 2007 near the middle of Norton Point (Figure 1c) and migrated east until it closed in 2015 (Figure 1d). While the inlet was open, the shoreline near the corner of Wasque Point eroded ~200 m [Figure 1d, compare the purple curve (2014) with the blue curve (2008, similar to 2007)]. Once Norton Point extended eastward and wrapped around Wasque Point, closing the inlet, the corner reverted toward its 2007 position [Figure 1d, compare the yellow curve (2015) with the blue curve (2008)]. Here it is shown that although the erosion and subsequent accretion of the southeast corner of Martha's Vineyard is consistent with a potential reduction (increase) in alongshore transport when the inlet is open (closed), the variability of transport (magnitude of erosion plus magnitude of deposition)

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24   depends strongly on the radius of curvature of the corner, a proxy for flow separation, which also

25   may impact the shoreline evolution.
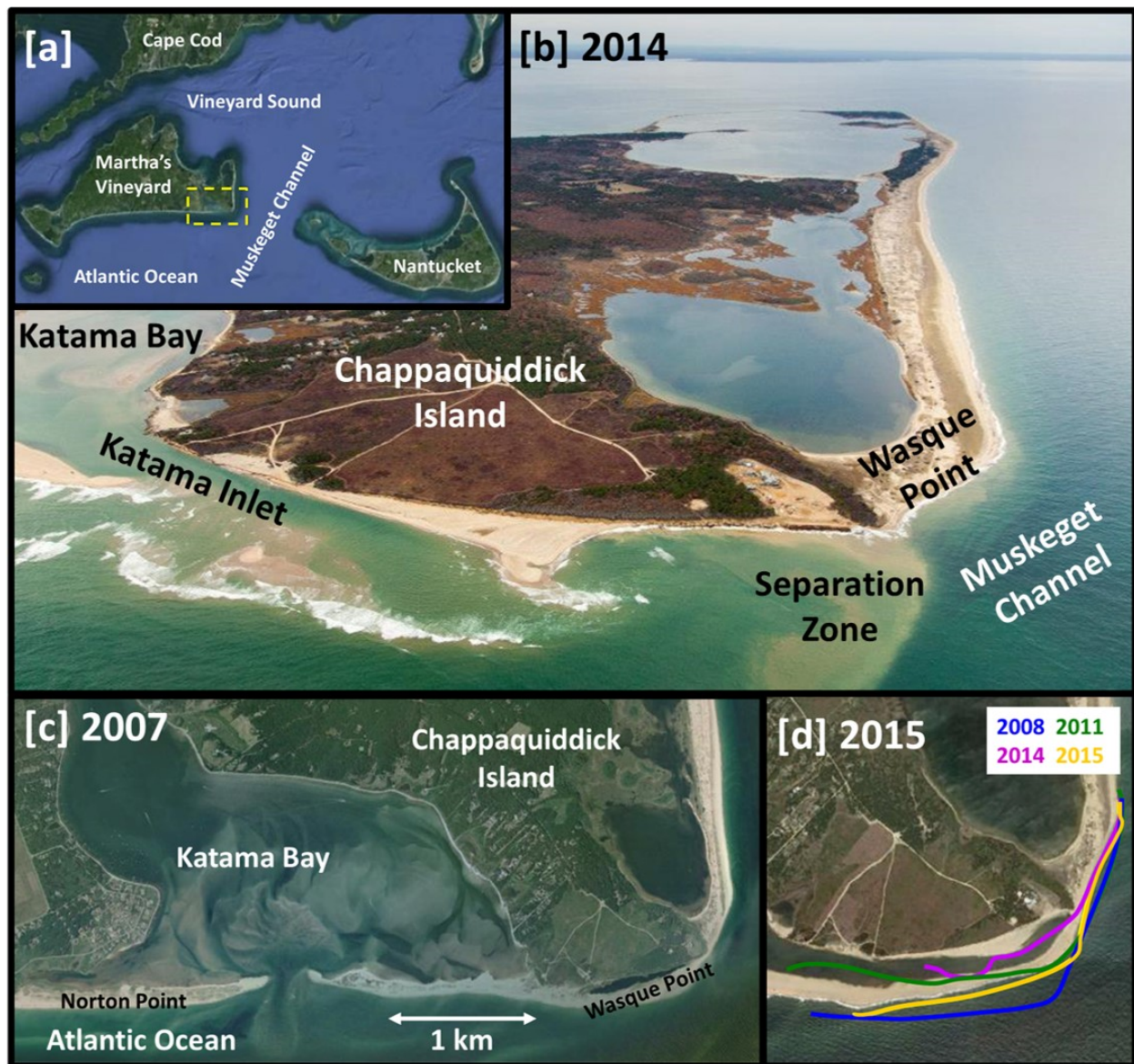
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27   **Figure 1:** (a) Location of Martha's Vineyard, MA, (b) photograph of Chappaquiddick Island,
28   Katama Bay and Inlet, and Wasque Point in 2014 [within the yellow box in (a)], (c) Google
29   Earth image of the Katama area 2 months after Norton Point was breached in Apr 2007, and (d)
30   close up image of Wasque Point in 2015, with shorelines from 2008 (blue curve, similar to
31   2007), 2011 (green), 2014 (purple), and 2015 (yellow). Photograph in (b) by Bill Brine.
32
33   Similar to the Martha's Vineyard coastline, many shorelines with inlets also have complex

34   larger-scale bathymetry and strong inner-shelf currents, including inlets throughout New

35   England [17], along the U.S. Atlantic Coast [18], and on sandy coasts around the world [12,19].

36 Strong currents near headlands or sharp shoreline transitions such as Wasque Point (Figure 1)

37 can impact sediment transport significantly. In particular, the separation of currents flowing

38 around headlands or sharp corners can generate eddies that suspend, transport, and deposit

39 sediment [18,20–23 and many others]. Flow separation and the generation of eddies depend on

40 the radius of curvature of the corner (or aspect ratio of a headland) [24], the balance of bottom

41 friction and current strength, and the ratio of flow strength to local acceleration [21]. Near

42 Wasque Point, the strong ebb jet through Muskeget Channel separates from the shoreline,

43 resulting in a quiescent zone at the southeastern corner of Chappaquiddick Island (Figure 1a,b).

44 The evolution of the radius of curvature of Wasque Point, a primary control of flow separation,

45 over the lifetime of Katama Inlet (Figure 1d) suggests that flow separation, in addition to the

46 inlet, could impact sediment transport at nearby shorelines. Here, field-tested numerical model

47 simulations are used to estimate the effects of an inlet, the ebb shoal, wave height, wave

48 direction, and shoreline geometry on erosion and deposition along a curved coast with a

49 migrating inlet.

50

51 **2. Numerical simulations**

52 Waves and currents were simulated with the numerical models SWAN (waves [25]) and

53 Delft3D-FLOW (currents [26]). The wave model solves the spectral action balance and includes

54 the effects of shoaling, refraction, and wave-current interaction. Similar to previous studies at

55 this location [27], for the no-wind cases and relatively short evolution distances here, wind and

56 nonlinear interactions were not included. The circulation model includes the effects of waves on

57 currents through wave radiation-stress gradients, combined wave and current bed shear stress,

58   and Stokes drift. The wave and flow models were coupled such that FLOW passes water levels

59   and Eulerian depth-averaged velocities to SWAN and SWAN passes wave parameters to FLOW.

60

61   SWAN was run with 36 10°-wide directional bins and 37 frequency bands logarithmically

62   spaced between 0.03 and 1.00 Hz. The model also used a depth-limited wave breaking

63   formulation without rollers [28], with the default value $\gamma = H_{sig}/h = 0.73$ (where the significant

64   wave height H_{sig} is 4 times the standard deviation of sea-surface elevation fluctuations, and h is

65   the water depth), and a JONSWAP bottom friction coefficient associated with wave-orbital

66   motions set to 0.10 m^2/s^3 [27].

67

68   The circulation model was run using the 13 most energetic satellite-generated tidal constituents

69   [29] along open boundaries, which were dominated by the M2 (~80% of the variance, with small

70   variation along the boundary) and N2 (~10% of the variance) constituents. In addition, the model

71   used a free slip condition at closed (land) side boundaries, a spatially uniform Chezy roughness

72   of 65 $m^{0.5}/s$ (roughly equivalent to a drag coefficient of $C_d = 0.0023$) at bottom boundaries, and

73   default Delft3D parameters for coupling the FLOW and WAVE models [30]. Second-order

74   differences were used with a time step of 0.15 s for numerical stability.

75

76   Sediment transport [31] was simulated using the modeled waves and currents. Model parameters

77   were set to default values with a grain size of 300 µm, except for the reference height (0.5 m),

78   the current-related reference concentration factor (0.25), and the wave-related suspended and

79   bed-load transport factors (0.1), which were reduced from the default values (1) that smoothed

80   all bedforms and produced unrealistic transport around the island. Transport was averaged over

81 several tidal cycles to remove variability within ebb or flood flows. The divergence

82 (convergence) of the transport vectors was used as a proxy for erosion (deposition), and the

83 morphology was not updated during the model run. These proxies primarily are a function of the

84 simulated hydrodynamics, which have been verified with field observations at this [27] and other

85 [10,32–35] shallow-water locations.

86

87 SWAN and Delft3D-FLOW (in depth-averaged mode) were run over 4 nested grids with both

88 two-way (FLOW) and one-way nesting (SWAN). The outermost grid, with 1 km resolution,

89 spans about 150 km along the north and south boundaries and 100 km along the east and west

90 boundaries. Nested in this coarse grid are finer grids of 200, 40, and 13 m resolution [27]. Using

91 higher resolution does not change simulation results significantly. Large-scale bathymetry within

92 the model domain was obtained during 1998 and 2008 USGS surveys (Northeast Atlantic 3 arc

93 second map [36] and Nantucket 1/3 arc second map [37]), and has horizontal resolution of 10 to

94 90 m. The bathymetry near the shoreline, inlet channel, bay, and ebb shoal near Katama Inlet

95 was obtained each summer between 2011 and 2015 with a GPS and an acoustic altimeter

96 mounted on a jetski. The horizontal resolution of the jetski surveys is on the order of 10 m, with

97 finer resolution near steep features. For 2008 (similar to 2007 immediately after the inlet was

98 breached), the location of the inlet and the geometry of the southeastern corner of

99 Chappaquiddick Island (Figure 1) were estimated from satellite images.

100

101 When initialized with frequency-directional spectra from WaveWatch III [38] along the offshore

102 boundary of the model domain, and run over the bathymetry observed in 2015, the model

103 simulates the currents observed near the southeastern shoreline of Chappaquiddick Island,

104   including the sharp gradient from the strong ebb flows in Muskeget Channel (red in Figure 2) to

105   the quiescent zone of weak flows near the shoreline (blue in Figure 2). The observed currents

106   were estimated with an acoustic Doppler current profiler (ADCP) mounted on a small boat. Each

107   suite of six transects (Figure 2a and 2b) took about 2 h, during which time the tidal flows

108   changed (increasing ebb currents flowing from Vineyard Sound to the Atlantic), explaining some

109   of the discrepancies with the 1-h flow simulations.
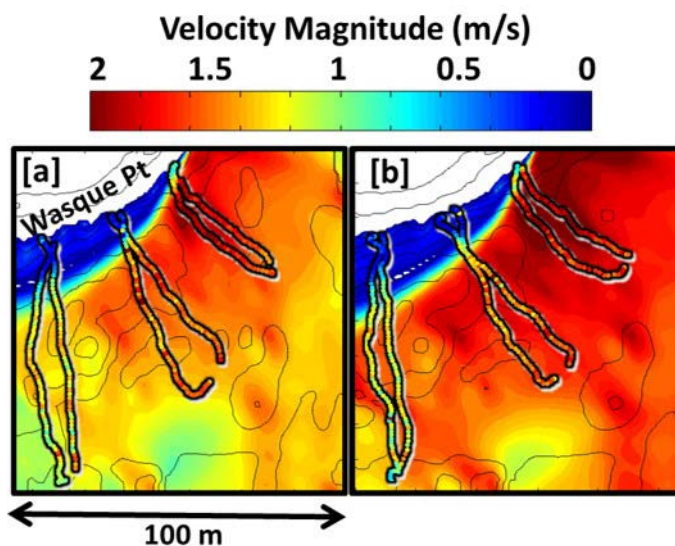
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111   **Figure 2.** Observed (colored symbols within black outlines of the boat transects) and simulated
112   (color contours, scale above) currents near Wasque Point during approximately (a) mid- and (b)
113   maximum-ebb tide. If model and data agree, the colors along the transect lines match the colors
114   of the surrounding simulation contours. The observations (13 Jul 2015) from the ADCP transects
115   are averaged over depth and over ~10 m along the track (boat speed ~1 m/s). The simulated
116   currents are from 1-h model runs initialized with wave and tidal conditions corresponding
117   approximately to those observed during the middle of each ~2-h long suite of transects.

118

3. Results and Discussion

120   Model simulations were used to investigate the effects of the inlet, the ebb shoal, incident wave

121   height, incident wave direction, and the shape of the southeast corner of Chappaquiddick Island

122   (a proxy for flow separation) on erosion and deposition of sediment near Wasque Point. Along

123   the offshore boundaries the model wave field had a JONSWAP spectral shape with $H_{sig} = 1$

124   (representative of typical conditions in this area occurring ~70% of the time in the last decade) or

8

125   3 m (representative of storm events that occur ~5% of the time) and 8 s waves with a $\cos^{20}$

126   directional distribution centered either on shore-normal or 30° west of normal. Tides on the

127   boundaries were set to values between spring and neap. Model simulations were averaged over

128   three tidal cycles for each year with observed nearshore bathymetry (2008, 2011-2015).
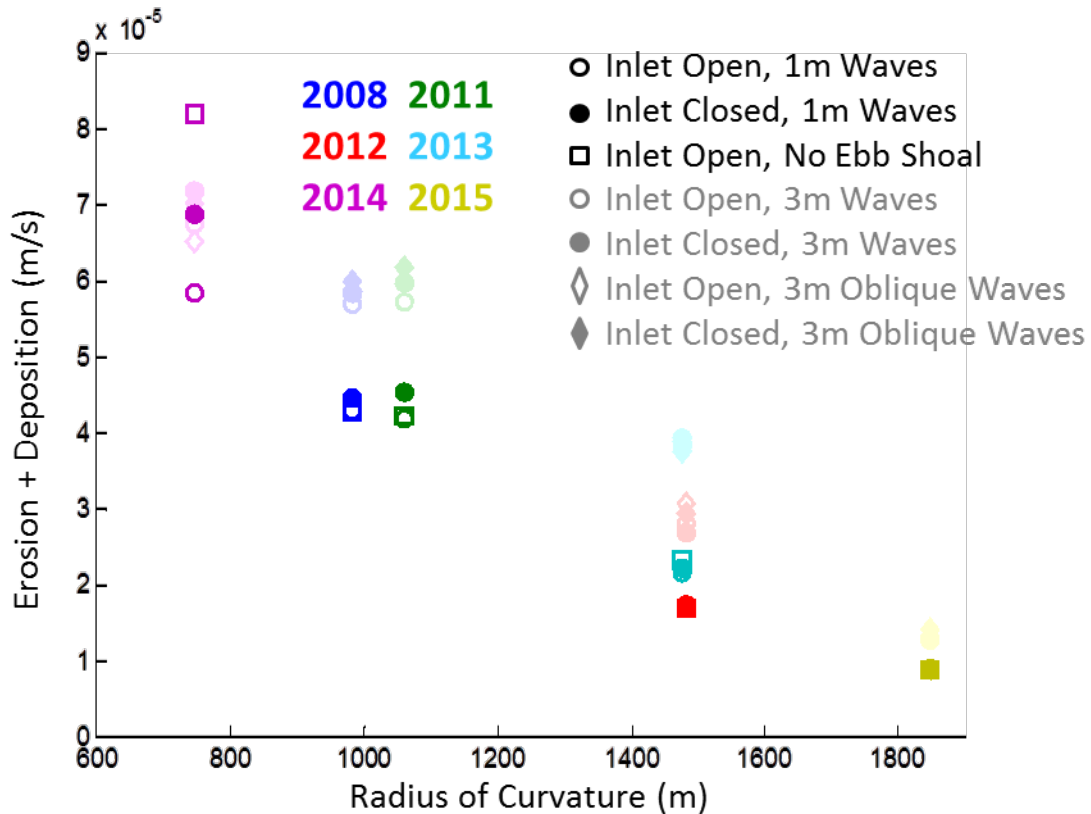
129

130   The radius of curvature of the southeast corner of Chappaquiddick Island is used as a proxy for

131   flow separation [24]. The center of the curve is at a point closest to where ebb flows begin to

132   separate from the shoreline, estimated as the location with the largest simulated cross-shore

133   velocity gradient near the corner (green circle in Figure 3a). The angles of tangents to the

134   shoreline (relative to the tangent at the center point) are calculated every 13 m on either side of

135   the center, and the slope of a least squares fit of distance as a function of angle is used as the

136   estimate of the radius of curvature (Figure 3b). The sum of the absolute values of total erosion

137   and total deposition within an area +/- 400 m from the center point extending from the shoreline

138   to 2-m water depth (Figure 3c) is used as a proxy for sediment transport. The results are not

139   significantly different for areas that extend between +/- 200 to +/- 500 m tangential to the center

140   and to 4-m water depth.

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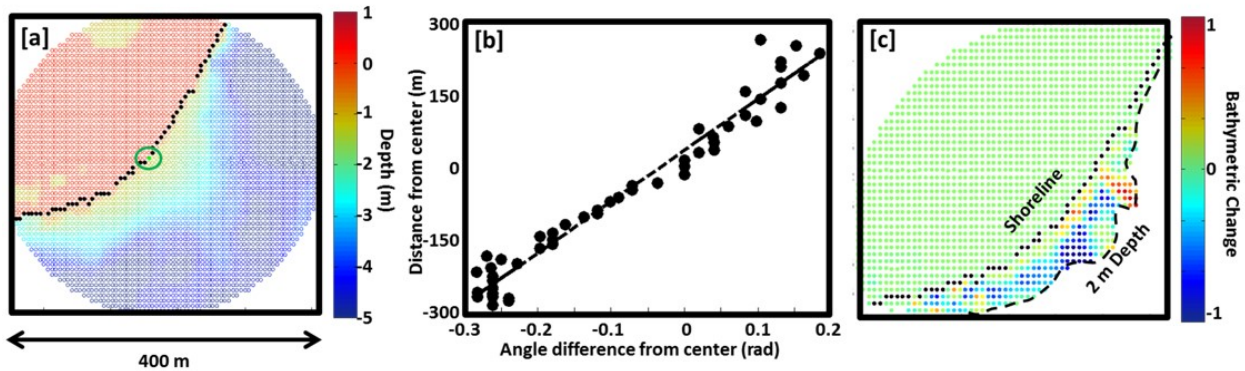
Figure 3: (a) Color contours of elevation (relative to mean sea level, scale on right) on the southeast corner of Chappaquiddick Island near Wasque Point in 2011. The black dots are the shoreline, and the green circle is the center of the radius of curvature. (b) Distance from the center point *versus* angle of tangents to the shoreline (relative to a tangent at the center). The slope of the least squares fit (dashed line) is the radius of curvature. (c) Color contours of erosion (blue) and deposition (red) (scale on right, arbitrary units) within a region between the shoreline (black dotted curve) and 2 m depth (black dashed curve).

Five scenarios were simulated for each of the 6 years with measured bathymetry. Erosion and deposition were estimated for 1-m high normally incident waves using *i*) the measured bathymetry (dark open circles in Figure 4), *ii*) the same bathymetry with the inlet artificially closed (dark closed circles on Figure 4), and *iii*) with the inlet open, but the ebb-tidal delta (ebb shoal) replaced with alongshore uniform bathymetry similar to that on either side of the shoal (open squares in Figure 4). In addition, erosion and deposition were simulated for 3-m high incident waves for each year using *iv*) the measured bathymetry with normally incident waves (light open circles in Figure 4), *v*) the measured bathymetry with normally incident waves and the inlet artificially closed (light closed circles, Figure 4), *vi*) the measured bathymetry with waves from 30° west of normal incidence (light open diamonds in Figure 4), and *vii*) the same bathymetry with the inlet artificially closed with waves from 30° west of normal incidence (light closed diamonds in Figure 4).

Figure 4. The sum of the absolute values of simulated erosion and deposition along 400 m of the shoreline between 0- and 2-m water depths (Figure 3c) *versus* the radius of curvature of the southeastern corner of Chappaquiddick Island in each of 6 years (colors, legend in upper right). Simulations used the bathymetry observed each year with the inlet open (open symbols), with the inlet artificially closed (closed symbols), with normally (circles) and obliquely (30° west of normal, diamonds) incident offshore wave directions, and with the ebb shoal removed artificially (open squares) for incident significant wave heights of 1 (dark colors) and 3 m (light colors). Inlet-open cases are not shown for 2015 because the inlet was closed.

Although momentum from the inlet flows during ebb tide tends to enlarge the separation region a

few tens of meters (not shown), the simulated total erosion and deposition is not strongly

affected by closing the inlet [compare open with closed circles for each year (colors) in Figure

4]. Similarly, removing the ebb shoal (Figure 4, open squares) does not have a significant effect

on erosion and deposition, except in 2014 (Figure 4, purple symbols) when the inlet mouth and

ebb shoal were < 0.5 km from Wasque Point (Figure 1b). Although as expected, there is more

sediment motion with 3 m waves than with 1 m waves with the inlet open or closed (Figure 4,

180 compare light with dark circles), and more transport with obliquely incident waves that drive

181 more alongshore flow (Figure 4, compare light diamonds with light circles), the differences in

182 erosion and deposition at the corner are relatively small. In contrast, the simulated erosion and

183 deposition depends more on changes in the radius of curvature than on the different scenarios in

184 any year (Figure 4), suggesting that sediment transport near the shoreline is influenced more by

185 separation from the coast of the strong Muskeget Channel ebb-tidal flows than on the presence or

186 absence of the inlet or the ebb shoal or on the details of the incident wave field.

187

188 The simulations further suggest that the geometry of the separation region and the intensity of

189 the separated jet combine to influence sediment transport at the southeast corner, and that the

190 vorticity generated at the boundary of the quiescent zone does not correlate to radii of curvature

191 or to erosion and deposition (not shown). Instead, tidally asymmetric transport is enhanced at the

192 shoreline when the corner is sharper (smaller radius) and the ebb-tide quiescent zone is larger,

193 because sediment is mobilized during the stronger flood flows and deposited during ebb when

194 currents decrease. The strength of the ebb jet outside of the quiescent zone also increases when

195 the corner is sharper, allowing for more sediment motion. In 2008, 1 year after Katama Inlet

196 formed, the radius of curvature was small and the simulations have relatively high erosion and

197 deposition near the shoreline (dark blue symbols in Figure 4). As the shoreline eroded between

198 2011 and 2013, the radius of curvature increased, and although the shoreline continued to erode,

199 satellite images suggest the rate slowed (not shown), consistent with the reduction in simulated

200 erosion and deposition (2011 through 2013 in Figure 4). In 2014 the inlet mouth was south

201 (rather than west) of Chappaquiddick Island (compare Figure 1b with 1c), and Norton Point had

202 extended eastward to within the separation region (Figure 1b), resulting in a greatly sharpened

203 corner (Figure 1b, purple symbols in Figure 4), and increased erosion and deposition. Between

204 summer 2014 (Figure 1b) and summer 2015 (Figure 1d) Norton Point extended rapidly (several

205 m/day from satellite and visual observations) until the inlet closed. When the Norton Point sand

206 spit reached the shoreline near Wasque Point in 2015, the corner was smooth (largest radius of

207 curvature), and erosion and deposition was smallest (yellow symbols in Figure 4), consistent

208 with visual observations that suggest the shoreline did not evolve significantly between 2015 and

209 2016.

210

211 Although the simulations suggest erosion and deposition near the shoreline do not depend

212 strongly on the presence or absence of the inlet, nor on wave-driven alongshore transport, there

213 is increased erosion downstream after the inlet opens, in contrast with a relatively stable

214 shoreline with the inlet closed (not shown). Disruption of alongshore transport or changes in

215 circulation when the inlet opens (e.g., the simulated tidally averaged momentum of the currents

216 near the southeast corner of Chappaquiddick Island decreases up to 10% when the inlet is open)

217 may enhance corner erosion and impact the strength of flow separation around the corner. Field-

218 verified simulations with evolving morphology might help determine why the shoreline starts to

219 erode when the inlet opens, and why the shoreline is stable when the inlet is closed. The

220 simulations here do not include morphological evolution. However, they suggest that erosion and

221 deposition decrease as the curvature of the southeast corner of Chappaquiddick Island increases

222 and separation from the coast of the strong Muskeget Channel ebb flows decreases.

Acknowledgements and data

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