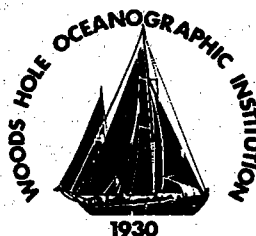


# Woods Hole Oceanographic Institution



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## Advanced Engineering Laboratory Project Summaries 1992

Edited by  
Daniel E. Frye

May 1994

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## Technical Report

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WHOI-94-14

Advanced Engineering Laboratory  
Project Summaries 1992

Edited by  
Daniel E. Frye

Woods Hole Oceanographic Institution  
Woods Hole, Massachusetts 02543

May 1994

**Technical Report**



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A handwritten signature in cursive script that reads "George V. Frisk". The signature is written over a horizontal line.

George V. Frisk, Chair  
Department of Applied Ocean Physics and Engineering

## **ABSTRACT**

The Advanced Engineering Laboratory of the Woods Hole Oceanographic Institution is a development laboratory within the Applied Ocean Physics and Engineering Department. Its function is the development of oceanographic instrumentation to test developing theories in oceanography, and to enhance current research projects in other disciplines within the community. This report summarizes recent and ongoing projects performed by members of this laboratory.

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# **ARCTIC UNDER-ICE SURVEY OPERATIONS**

**James G. Bellingham, Max Deffenbaugh, John J. Leonard,  
Josko Catipovic and Henrik Schmidt**

## **ABSTRACT**

This paper describes the challenges of designing an autonomous underwater vehicle system for surveying the underside of the Arctic ice canopy. The operations are in support of an Arctic sea ice mechanics research program sponsored by the Office of Naval Research. The objective is to launch and recover an autonomous underwater vehicle through the ice to make measurements of the topography of the underside of the ice canopy. Transits of up to ten kilometers and mapping operations over an area of one square kilometer are desired. The vehicle, a modified version of the Odyssey AUV, is presently under construction and will be operated in the Arctic in spring of 1994.

Funding was provided by Office of Naval Research under contract N00014-92-J-1287 and the Massachusetts Institute of Technology Sea Grant College Program under contract NA90AA-D-SG424.

Published in: Proceedings 7th International Symposium on Unmanned Untethered Submersible Technology, University of New Hampshire, September 1991.

# LASER SLOPE GAUGE LENS DESIGN AND OPTIMIZATION FOR SMALL SURFACE WAVE MEASUREMENTS

Erik Bock and Robin Singer

## ABSTRACT

A lens design program has been written to optimize the detector of a laser wave-slope gauge, built at W.H.O.I. and tested in lab and field experiments. The gauge determines the two dimensional spectra of waves on the surface of the ocean. Careful detector design can minimize systematic errors and increase the accuracy of local surface slope measurements.

The gauge makes use of a laser light source that scans the water surface. The laser beam is deflected by refraction through the water-air interface where the local surface slope varies owing to the presence of waves. Once the beam is deflected, the optical receiver resolves the amount of deflection by determining the two orthogonal components of angular deflection.

The main errors introduced into the measurement scheme include the system's sensitivity to the relative distance between the water surface and the detector, nonlinearities intrinsic to the beam-sensing electronics, and asymmetries associated with the fact that the origin of the deflected beam is not on the optical axis of the system. Lens simulation software, that specifies the performance of an aspheric lens by means of exact ray tracing techniques, has been developed to minimize the error introduced by these effects. An optimal lens is designed by randomly altering the lens surfaces until the lens performance minimizes a set of error parameters derived as a measure of the systematic errors described above.

## Motivation

Laser slope gauges are routinely used to measure the small-scale wave structure associated with short water-surface waves. These waves are capillary and capillary-gravity waves (ripples) that have characteristics that are modified by oceanographic processes, including marine surfactant, subsurface currents, and variations in wind stress. Slope gauges rely on the refraction of a pencil-like laser beam at a point at the air-water interface that has a local slope owing to the presence of a wave. The amount of angular refraction can be related to the quantity-of-interest (i.e. the water slope) through Snell's law, given as:

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

where  $n_1$  is the index of refraction of water,  $n_2$  is the index of refraction of air,  $\theta_1$  is

the angle between the incident laser beam and the surface normal of the air-water interface and  $\theta_2$  is the angle between the refracted beam and the surface normal of the interface. It is then convenient to measure the amount of angular refraction of the laser beam as it passes through the air-sea interface.

In the simplest case consider a water surface that has above it, a fixed flat screen that is in a plane parallel to the mean water surface. For low-amplitude waves, the location of the beam, after it has traveled away from the water surface and hit the screen, serves as an adequate approximation for the instantaneous local slope. When wave heights become significant, this simple approximation becomes invalid, because the distance between the water surface and the screen varies.

Since the small waves of interest (waves with wavelengths from a few millimeters to tens of centimeters) ride on the larger waves that can have wavelengths of tens of meters and amplitudes of several meters or more, we make use of a floating platform to deploy our slope gauge. The platform (a 6 m research catamaran named LADAS) follows the ocean surface so that the instrument mounted at the bow of the catamaran stays within 60 cm of the ocean surface. The detector is operated on the air-side of the interface. It makes use of an aspheric lens, designed with the first generation of the software described in this paper, to reduce errors associated with the residual height variations resulting from imperfect wave-following on the part of the catamaran.

### **Instrument description**

The instrument makes use of an aspheric lens, an optical scattering element, and analog detection electronics to determine laser deflection in the range of  $\pm 13$  degrees, with the origin of deflection varying in distance from the detector. The nominal distance between the water surface and the detector is 60 cm ( $\pm 30$  cm). The instrument was successfully deployed in several laboratory and field experiments here at Woods Hole, at the Canada Centre for Inland Waters (CCIW), and off Cape Hatteras as part of the High Resolution ARI pilot and main field experiments.

### **Lens design software**

The software was written to find an optimal lens with minimal spread and linear errors, as defined below. These error values indicate the accuracy of the optical systems:

Spread error is defined as the sum of the standard deviations of the distances,  $r$ , at the focal plane, from its center (the optical axis), of rays of differing incidence angle,  $\theta$ , that had origin at different starting distances,  $z$ , from



the lens and at different orientation angles,  $\phi$ . Formally, it is defined as:

$$\frac{1}{n_{\theta}} \times \sum_{\theta=0}^{\theta_{\max}} \sqrt{\frac{1}{n_{\phi z}} \times \sum_{\phi=0}^{2\pi} \sum_{z=z_{\min}}^{z_{\max}} (r - \mu_r)^2}$$

where  $\mu_r$  is the mean of the  $r$  values,  $n_{\phi z}$  is the number of rays per incident angle, and  $n_{\theta}$  is the number of incident angles.

Linear error is defined as 1 minus the regression coefficient for the same set of rays using the linear regression between distance from center at the focal plane,  $r$ , and the angle of incidence,  $\theta$ ; it is given as:

$$1 - \left[ \frac{1}{n_{\theta}} \times \sum_{\theta=0}^{\theta_{\max}} \left( \frac{m_{r\theta} - \overline{m_{r\theta}}}{\sigma_m} * \frac{\theta - \overline{\theta}}{\sigma_{\theta}} \right) \right]$$

where  $m_{r\theta}$  is the mean of the distances ( $r$ ) for a given angle  $\theta$ , and  $\overline{m_{r\theta}}$  is the mean of those means,  $\sigma_m$  is the standard deviation of the means,  $\overline{\theta}$  is the mean of the angles,  $\sigma_{\theta}$  is the standard deviation of the angles, and  $n_{\theta}$  is the number of incident angles.

Spread error is proportional to the degree of scatter of the rays, and linear error is proportional to the nonlinearity of the relation between incoming angle and the amount of displacement at the focal plane.

The program starts by reading a lens data file, which contains the coefficients of two twelfth order polynomials that describe the upper and lower surfaces of a lens, the working focal length which is allowed to vary in the current strategy, and the previously calculated best value of spread error and linear error. Two of the lens coefficients are randomly permuted in order to describe a new lens. The new lens must pass a set of tests in order to determine if it is physically realizable and if it is, rays are traced through the new lens to a set of positions on the focal plane. This enables the calculation of spread and linear errors which are used for determining the accuracy of the optical system.

If either error value is lower than the recorded error values for the previous lens, the lens coefficients and focal length are written to a data file along with the improved error value. Lens parameters producing a better spread error are used for future iterations. The range of distances and the ranges of incident angle and orientation are all specified by the lens designer. The ray tracing is accomplished in three dimensional geometry, using the three dimensional extension of the Newton-Raphson method for finding intercepts, and applications of Snell's Law. The spread error calculation is based on the standard deviation of the universe, not the sample standard deviation. The minimum and maximum lens thickness, the lens' radius, and the index of refraction are specified as constants and can be easily modified. A modification of this code and some Matlab "M" files permit the generation of plots of the locations at which the rays strike the focal plane. These plots enable the lens designer to evaluate the performance of the lens, and to determine when an acceptable design has been achieved.

### **Software use**

The code has been used on a 20 MHz 386 PC and will converge to an optimized lens in an overnight run. The optimized parameters in the data file can be used as specifications to Applied Products Corporation, located in Bristol, Pennsylvania, who can machine an acrylic lens from them. For use in the laser-slope gauge, the lens is covered with a tinted (red) acrylic plate and the contact area between the plate and lens is oil-filled with silicone fluid to match the index of refraction and prevent satellite reflections at multiple air/acrylic interfaces.

After a new lens has been chosen, it will be fabricated and tested with lasers in the laboratory to evaluate its performance. It is anticipated that it will be incorporated in laboratory experiments in Heidelberg, Germany in October of 1994, and in future field experiments.

### **Conclusion**

By simulating the path of rays through randomly generated, simulated lenses, a lens can be found that improves the performance of a limited range laser-slope gauge. This will aid in the characterization of the capillary and capillary-gravity waves at the surface of the ocean.

Funding was provided by Office of Naval Research under Contract N00014-90-J-1717.

# **ROBUST MULTIUSER COMMUNICATION FOR UNDERWATER ACOUSTIC CHANNELS**

**David Brady and Josko Catipovic**

## **ABSTRACT**

This paper presents a method for easing acoustic channel congestion present whenever multiple acoustic systems or multiple UUVs are sharing acoustic bandwidth. We consider the acoustic environment as a multiuser network, where multiple systems (users) need to operate synchronously, with minimal regard for other channel users. In many multipoint random access networks, the collision of data packets from two co-channel and asynchronous transmitters is viewed as unresolvable. Network protocols are usually designed to avoid and discard packet collisions, and to utilize a side channel for retransmission requests to both transmitters. This paper presents a random-access communication network capable of resolving collisions between several asynchronous and co-channel packets without side channel communication.

The algorithm differs from standard capture schemes by demodulating the data from both strong and weak transmitters. The resulting acoustic network protocol requires roughly the same transmission bandwidth as other networks at the expense of an increased computational complexity at the receiver processor. Examples are given and illustrate that this technique is extremely desirable for underwater acoustic local area networks and underwater autonomous vehicles with both side-scan sonar as well and acoustic telemetry links.

Funding was provided by National Science Foundation under Contract OCE92-01191.

Published in Proceedings IEEE Unmanned Underwater Vehicle Conference, June 1992.

# **THE ANNUAL EVOLUTION OF GEOSTROPHIC FLOW IN THE GULF OF MAINE: 1986-87**

**Brown, W. S. and J. D. Irish**

## **ABSTRACT**

The evolution of geostrophic flow in the Gulf of Maine has been documented using five water property surveys conducted during the thirteen-month period of moored observations in 1986-1987. The scales of mesoscale flow decreased from 100-200 km during winter to 50-100 km in late summer - apparently related to an evolving water mass structure. The basin-scale geostrophic transport around Jordan Basin underwent several reversals during the year, ending with a weak counterclockwise Gulf of Maine gyre in September 1987.

Published in *Journal of Physical Oceanography*, 22(5), 445-473, 1992

Funding provided by National Science Foundation under contract OCE 8818060 and NOAA Sea Grant Program.

# **INTEGRATED CTD OCEANOGRAPHIC DATA COLLECTION PLATFORM**

**Alan J. Fougere, Neil L. Brown, Edward Hobart**

## **ABSTRACT**

The Mark II conductivity-temperature-depth (CTD) profiler has been a mainstay of modern physical oceanographic research. The MKIIIB CTD provides high quality oceanographic data when used by skilled personnel and require frequent recalibration. The design objective of the Integrated CTD system was to attain the same high level of performance while reducing the necessity of frequent recalibration through the enhancement of long term stability. This goal required consideration of both the electronic approach and the re-design of the physical sensors. The result of this work is a CTD system with improved measurement precision. All three primary sensors are newly designed to achieve long term measurement stability and to optimize system sampling performance without the limitations of existing technologies.

Advances in the state of the art in electronic and microcontroller technologies has enabled the development of improved methods of analog sensor signal processing. The revolution in high speed microcontrollers has allowed their use in the Integrated CTD allowing for real time numerical correction for drift in the analog signal processing circuitry.

Funding provided by Woods Hole Oceanographic Instrument Initiative under project #33423300.

Published in Proceedings Oceanology International '92, Brighton, England, March 1992.

# TELEMETRY CONCEPTS FOR DEEP SEA MOORINGS

Daniel E. Frye and Henri O. Berteaux

## ABSTRACT

To expand the state of the art in moored array technology, Woods Hole Oceanographic Institution (WHOI) is pursuing a series of engineering tests conducted from buoys moored offshore Bermuda. Assessment of new sensors and data transmission techniques are included in the evaluation of new buoy and mooring components of markedly improved performance as are measurement of buoy system dynamics, and long term exposure of new materials.

Reasons for selecting Bermuda as the test site included proximity to deep water, the facilities for staging and monitoring the experiment (Bermuda Biological Station for Research), an abundance of winter storms and an occasional hurricane, a good collection of epipelagic and mesopelagic predators, and availability of the R/V Weatherbird. The site duplicates the hostile conditions encountered in many other remote parts of the Atlantic.

The experimental work involves the long-term (18 month or more) exposure of components and a systematic evaluation of their performance in situ. Degradation due to corrosion, fatigue, fouling, fishbites, etc., is carefully monitored as a function of depth and time.

Results of the engineering surface oceanographic mooring (ESOM) experiment in 1989-1990 were discussed in *Sea Technology* (February 1992). ESOM was also used as a platform from which to conduct the full-scale, in situ evaluation of an underwater acoustic telemetry system developed by Dr. Josko Catipovic and engineers in the Advanced Engineering Laboratory at WHOI (*Sea Technology*, May 1990).

A second experimental mooring, ALTOMOOR (Atlantic long term oceanographic mooring), will be deployed offshore Bermuda in 1993. In addition to the continued testing of moored array components, this mooring will be used to acquire a comprehensive set of mooring dynamic measurements, to assess the performance of a new acoustic current meter developed by Neil Brown of WHOI and finally to evaluate inductive coupling techniques for underwater telemetry.

Funding provided by Office of Naval Research. Moored Array Technology is supported by Dr. S. Ramberg, director of the Ocean Engineering Division, contract No. N00014-90-J-1719. Telemetry development was supported by Dr. D. Evans under contract No. N00014-86-K-0751.

Published in *Sea Technology*, May 1992.

# NOISE TESTS ON THE VALIDYNE DIFFERENTIAL PRESSURE SENSOR - Technical Memorandum

John T. Hallinan

Several tests were carried out in order to determine if the Validyne DP15-34 Differential Pressure Sensor is capable of resolving 10 Pascal while maintaining a full scale capability of 22,000 Pascal. The 16 bit AtoD and the 4 Pole low pass filters from the ONR OBS were used to make the measurements. Figure 1 describes the setup.

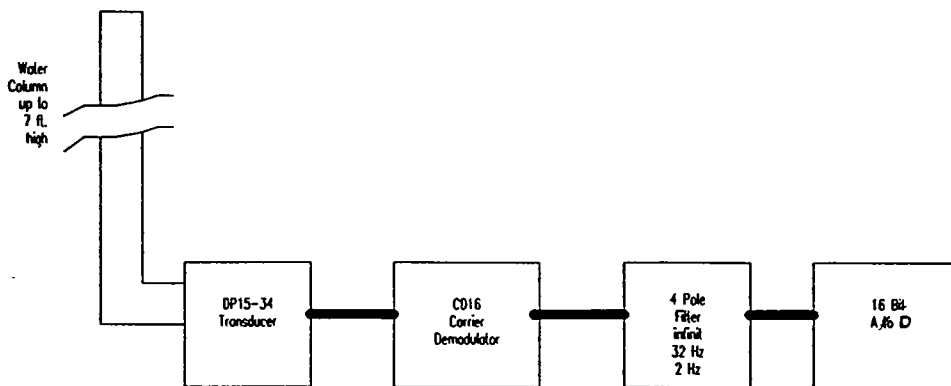


Figure 1

The plotting program is described below.

1. The plot program determines the maximum and minimum values in the data set that it will plot and compresses the vertical scale so the wave form fills the complete screen. It does this for each iteration of the plot and when the zoom feature is used the scale will change.
2. The program compresses the horizontal scale so that the data set fills the full screen. The zoom feature will also change this scale.

3. The numbers in the upper right corner of the plot are the maximum and minimum values contained in the data set. The units are number of LSBs of the 16 Bit Bipolar AtoD. The full scale range is 32767 to 32768. The program prints the maximum and the minimum values and computes the difference to plot the peak to peak value.
4. A conversion factor of  $.000146lb \cdot in^{-2} = 1Pa$  is used in the calculations.
5. The system was calibrated by raising the height of the water in the water column approximately seven feet above the transducer and adjusting the span of the CD16 to give five Volts input to the AtoD.

Fresh water was used which has a density of  $62.4lb \cdot ft^{-3}$ .

$$62.4lb \cdot ft^{-3} \div 144in^2 \cdot ft^2 = .433333lb \cdot ft^{-1} \cdot in^{-2}$$

$$22,000 Pa \times .000146lb \cdot in^{-2} \cdot Pa^{-1} = 3.212lb \cdot in^{-2}$$

$$3.212lb \cdot in^{-2} \div .433333lb \cdot ft^{-1} \cdot in^{-2} = 7.41ft$$

which means that the full scale reading of the AtoD, 32767 LSBs is approximately 22 KPa and each bit has a weighting of 0.671387uPa

$$22,000Pa \div 32,768Bits = 0.671387Pa \cdot Bit^{-1}$$

The Validyne Carrier Demodulator CD16 furnishes a 5 KHz square wave to the DP15-34 transducer to excite the coils and the CD16 demodulates the transducer signal to a DC output. Therefore there is a high probability that the 5 KHz will find its way into the data. The first test set the 4 pole filter pass band to infinity (i.e. no filter), the level of the water in the water column was zero inches, the sample rate was 128 samples per second. Figure 2 is a plot of the data collected. Independent readings from an oscilloscope showed the 5 KHz was riding on the analog signal but that the level was on the order of 7 mV peak to peak which is within the ripple specification for the CD16. Figure 2 shows the effect of the 5 KHz beating against the 128 Hz Sample rate.

The data in Figure 2 has a peak to peak pressure differential of  $455 Bits \times 0.671387Pa \cdot Bit^{-1} = 305.5Pa$ .



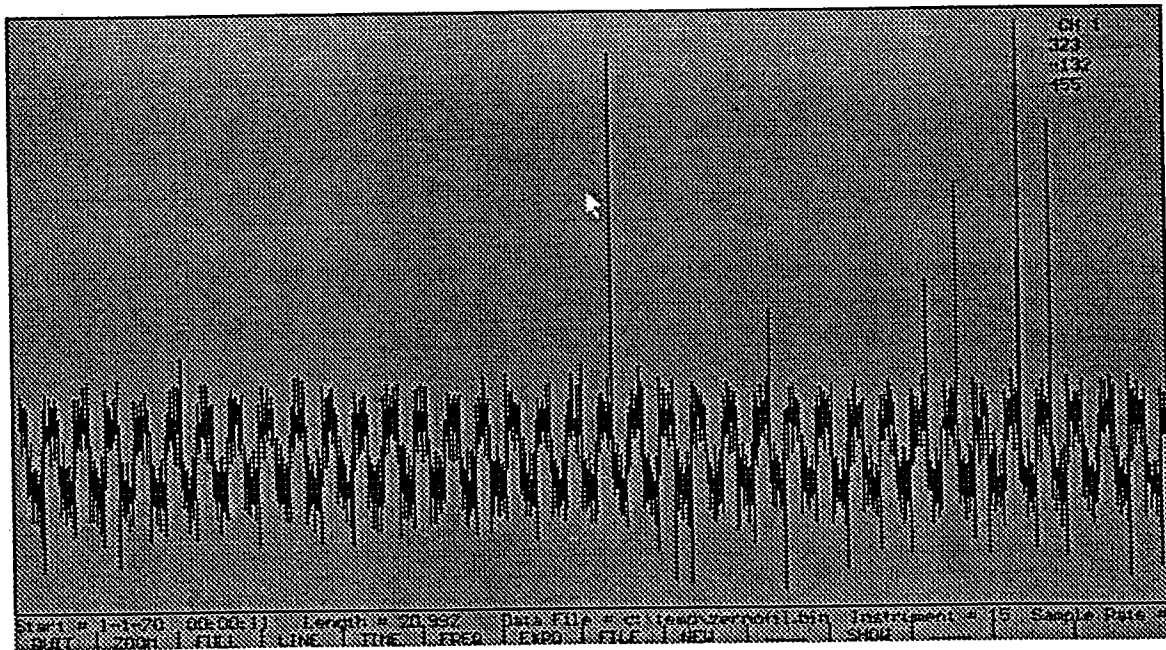


Figure 2

However, this differential is skewed by several single sample spikes. Figure 3 shows a zoomed plot of the same wave form without the spikes. This section of data has a peak to peak differential of  $143\text{Bits} \times 0.671387\text{Bits} \cdot \text{Pa}^{-1} = 96\text{Pa}$ , which is ten times as much as we are trying to resolve.

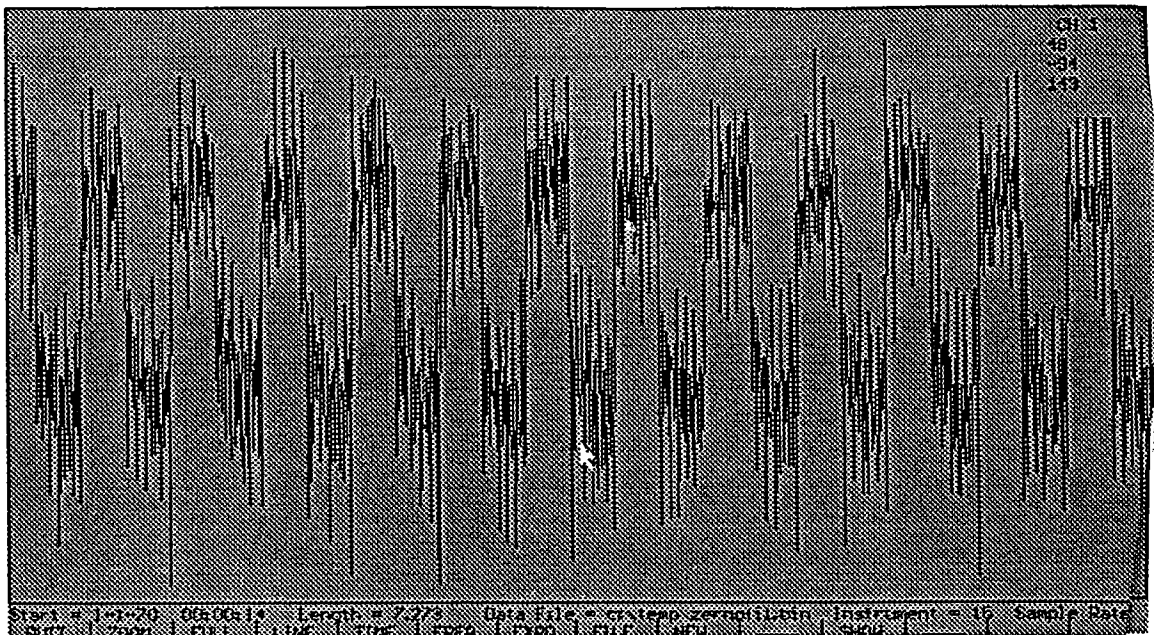


Figure 3

