

WebPanel 1. A model for scaling denitrification to river networks

We developed a model of NO_3^- loading, transport, and denitrification in stream and river networks (described in detail by Mulholland et al. 2008) to scale up empirical measures of stream-reach denitrification. The model is based on a steady-state, mass-balance approach and hydrogeomorphic scaling principles commonly used to represent river geomorphology and hydrology, including: (1) steady-state hydrologic flux; (2) accumulation of water in streams and rivers from their drainage areas as they flow downstream; (3) uniform water yield for each sampled subcatchment (see Figure 2); and (4) channel width increasing downstream in proportion to discharge. In accordance with typical river-network model assumptions, denitrification is the primary nitrogen removal pathway (Wollheim et al. 2006).

The model calculates denitrification within stream segments and routes water (Q ; $\text{m}^3 \text{d}^{-1}$) and NO_3^- (NO_3 ; g d^{-1}) between segments linked together into networks (see Figure 1). Upstream inputs to a stream segment (i) of water (Q_{ui}) and NO_3^- ($\text{NO}_{3,ui}$) are equal to the sum of exports from upstream segments.

$$Q_{ui} = \sum(Q_{i-1}) \quad (\text{Eq 1}) \qquad \text{NO}_{3,ui} = \sum(\text{NO}_{3,i-1}) \quad (\text{Eq 2})$$

Lateral water (Q_{Li}) and NO_3^- ($\text{NO}_{3,Li}$) inputs from the terrestrial landscape are equal to the product of the area draining directly to stream segment i (A , m^2) and the area specific loading rate (Y) of water ($\text{m}^3 \text{m}^{-2} \text{d}^{-1}$) and NO_3^- ($\text{kg m}^{-2} \text{d}^{-1}$).

$$Q_{Li} = A_i Y_{Qi} \quad (\text{Eq 3}) \qquad \text{NO}_{3,Li} = A_i Y_{\text{NO}_3i} \quad (\text{Eq 4})$$

We calculated downstream exports using a steady-state mass-balance approach where downstream fluxes of water (Q_{ei}) and NO_3^- ($\text{NO}_{3,ei}$) equal the sum of inputs minus outputs.

$$Q_{ei} = Q_{ui} + Q_{Li} \quad (\text{Eq 5}) \qquad \text{NO}_{3,ei} = \text{NO}_{3,ui} + \text{NO}_{3,Li} - \text{NO}_{3,Ri} \quad (\text{Eq 6})$$

$\text{NO}_{3,Ri}$ is the NO_3^- removed from stream segment i via denitrification, and is the product of the fraction of NO_3^- denitrified (R) and the sum of NO_3^- inputs to the segment.

$$\text{NO}_{3,Ri} = R_i(\text{NO}_{3,ui} + \text{NO}_{3,Li}) \quad (\text{Eq 7})$$

The fraction of NO_3^- denitrified from each stream segment is determined by:

$$R = 1 - e^{-v_{\text{den}}/H_L} \quad (\text{Eq 8})$$

where hydraulic load (H_L , m s^{-1}) is the ratio of discharge to streambed surface area (length times width of each stream segment; Wollheim et al. 2006). Stream length was determined from USGS stream hydrography data (1:24 000). Stream width (w) was calculated using modeled discharge (Q) for each stream segment (Leopold and Maddock 1953):

$$w = aQ^b \quad (\text{Eq 9})$$

Parameters a and b were estimated empirically for low-flow conditions within each catchment (WebTable 1). Because water yields and width parameters were derived from low-flow measurements, the model scenarios apply to low-flow conditions within each catchment.

Conceptually, uptake velocity for denitrification (v_{den}) is the downward velocity of NO_3^- molecules through the water column necessary to meet observed streambed denitrification demand for NO_3^- . Mulholland et al. (2008) demonstrated that v_{den} decreases with increasing in-stream NO_3^- concentration ($[\text{NO}_3]$), following a power function. Thus, the model determines v_{den} for each stream segment according to:

$$v_{\text{den}} = c [\text{NO}_3]^d \quad (\text{Eq 10})$$

We derived parameters c and d empirically for each catchment using observed values of v_{den} and $[\text{NO}_3]$ from 5–9 experimental stream reaches located within or adjacent to each modeled network (WebTable 1).

WebTable 1. Site-specific parameter values for river-network modeling

Site abbreviation	Channel width a, b (r^2)	Uptake velocity (v_{den}) c, d (r^2)
NC	7.3, 0.45 (0.90)	8.2E-1, -1.2 (0.72)
KS	7.2, 0.35 (0.74)	2.3E-4, -0.48 (0.61)
OR	7.2, 0.35 (0.74)	7.6E-1, -1.2 (0.18)
WY	7.0, 0.33 (0.50)	8.5E-1, -0.10 (0.88)
MA	7.4, 0.27 (0.37)	4.0E-4, -0.47 (0.60)
MI	10.4, 0.45 (0.93)	1.1E-1, -0.93 (0.53)
PR	6.6, 0.35 (0.27)	3.4E-6, -0.063 (0.01)
NM	nd	4.2E-5, -0.36 (0.23)

Notes: The width coefficient (a) and exponent (b) were used to determine channel width for each stream segment (using Eq 9 in WebPanel 1). The denitrification coefficient (c) and exponent (d) were used to determine denitrification uptake velocity (v_{den}) for each stream segment (using Eq 10 in WebPanel 1). nd = no data.

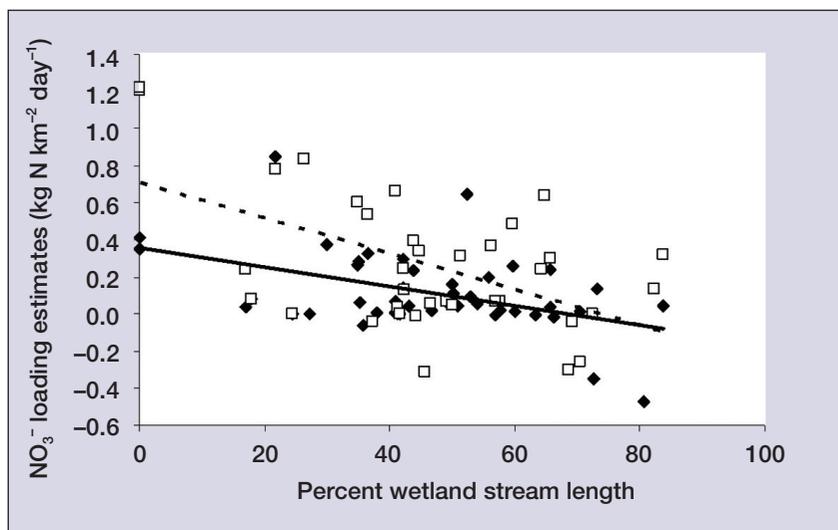
WebTable 2. Literature review used to determine the realistic range of modeled NO₃⁻ loading estimates

Location	Number of catchments	Catchment area (km ²)	% agriculture	% urban	Loading estimate (kg N km ⁻² d ⁻¹)	Method used to estimate loading	Reference
Loch Vale Watershed, Colorado Front Range	1	6.6	0	0	0.69	Modeled direct total N loading to aquatic ecosystems	Baron and Campbell (1997)
Upper Mississippi	3	492 000 (422 000–1 320 000)	nd	nd	1.93 (0.28–2.52)	Measured NO ₃ ⁻ river export	Carey <i>et al.</i> (2001)
Embarrass River, Illinois	1	482	91	4.5	6.54	Measured NO ₃ ⁻ river export	David <i>et al.</i> (1997)
Gwynns Falls, Maryland	3	0.32 (0.08–0.81)	0 (0–100)	0 (0–47)	1.78 (0.14–4.49)	Measured total N river export	Groffman <i>et al.</i> (2004)
Lake Michigan basin	18	2398 (153–15 825)	42 (5–82)	2 (0.2–20)	0.86 (0.47–3.63)	Measured total N river export	Han <i>et al.</i> (2009)
Southeast US	14	2125 (63–56 894)	16 (2–42)	0.5 (0.05–5)	1.30 (0.71–2.50)	Measured total N river export	Harned <i>et al.</i> (2004)
LTER sites across North America	13	0.38 (0.06–10)	nd	nd	0.19 (0.03–1.18)	Measured dissolved inorganic N river export	Kane <i>et al.</i> (2008)
Oldman River, Alberta, Canada	1	28 200	nd	nd	0.76	Measured total N river export	Rock and Mayer (2006)
US West Coast	18	8995 (1531–279 438)	6 (0.4–24)	1 (0–20)	0.32 (0.19–4.57)	Measured total N river export	Schaefer <i>et al.</i> (2009)
Sierra Nevada and Rocky Mountains	28	1.6 (0.2–19.1)	nd	nd	0.20 (0.008–0.85)	Measured dissolved inorganic N river export	Sickman <i>et al.</i> (2002)
Central Valley, California	23	2736 (461–61 721)	6 (0–74)	2 (0–6)	0.31 (0.06–2.59)	Measured total N river export	Sobota <i>et al.</i> (2009)
Northeast US	16	11 945 (475–70 189)	10 (1–61)	3 (0–22)	5.51 (2.74–6.96)	Modeled estimates of NO ₃ ⁻ leaching to ground and surface waters	Van Breeman <i>et al.</i> (2002)
Ipswich River basin, Massachusetts	1	404	7	35	1.85	Estimated direct total N loading to river network by 1st-order streams	Williams <i>et al.</i> (2004)
Summary	140	1791 (0.06–1 320 000)	10 (0–100)	1.2 (0–47)	0.49 (0.008–6.96)		

Notes: Catchments in the literature review span a wide range of geographic regions, catchment areas, and land-use conditions. When references included more than 1 year of loading data for a particular catchment, the average value was used. Data are reported as median (range). The highest reported nitrogen loading rate was 6.96 kg N km⁻² d⁻¹. nd = no data.

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WebFigure 1. Modeled NO_3^- loading estimates from the Ipswich River, MA, versus upstream percent wetland stream length (ie ratio of stream length passing through wetlands to total stream length). Wetland extent determined from 2001 National Land Cover Dataset (<http://seamless.usgs.gov>). Loading estimates derived from network modeling were negatively correlated with percent wetland stream length for both years of estimated loading rates (2003 $r^2 = 0.21$, $P < 0.002$, solid line and diamonds and 2004 $r^2 = 0.31$, $P < 0.002$, dashed line and open squares), suggesting that the model underpredicts denitrification in channels flowing through wetlands.